Investigation of the Non-adiabatic Thermoelastic Effect in Face-sheet/core Debonded Composite Sandwich Structures

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Motivation

Composite Sandwich Structures

• High bending stiffness and strength to weight ratio















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Background

Damage in sandwich structures

- Reduce stiffness and strength
- **Previous studies**
- Crack tip
- Subsequent damage propagation at the face-sheet/core interface can be identified

Large structures

• Difficult to access and view hidden damaged area



Martakos et al [1]



[1] Martakos G, Andreasen J, Berggreen C, Thomsen O. Experimental investigation of interfacial crack arrest in sandwich beams subjected to fatigue loading using a novel crack arresting device. Journal of Sandwich Structures & Materials. 2019;21(2):401-421. doi:10.1177/1099636217695057









Aims/Objectives

Investigate the non-adiabatic thermoelastic response at the facesheet/core interface in sandwich beams

- Assessing defect severity through through-thickness view
- Model validation using experimental data
- Investigating heat transfer at the interface using numerical models and experimental data







Thermoelastic stress analysis (TSA)

TSA utilizes the thermoelastic effect to correlate the temperature variations and the stresses in a structure subjected to elastic cyclic loading









Non-adiabatic thermoelastic response

Multidirectional carbon fibre composites

- High thermal gradients
 - Heat transfer at low loading frequencies
- Subsurface plies influence the temperature at the surface

Identified interface debond regions

- Through the face-sheet
- Non-adiabatic thermoelastic response

Can this be related to the damage severity at the interface?







Experimental methodology

- Face-sheet unidirectional CFRP
- Core PVC
- Teflon film is used to create debonded region
- Loading: -500N ± 400 N
- Frequency: 1 11 Hz











Thermoelastic responses at through-thickness view



Two high ΔT areas at the core
ΔT increases with loading frequency
Distance between high ΔT areas ≈ debond size
Low signal at the face-sheets and core









Phase at through-thickness view



Top face-sheet in compression Bottom face-sheet in tension

Face-sheets ≈ opposite in phase as the loading frequency increases









ΔT and Phase





Modelling details

Geometric non-linear model

Element type

- C3D20RT-20-node coupled temperature-displacement elements (face-sheet and core)
- Global element size = 1.5 mm
- Refined element size at the debonded region= 0.4 mm

Total number of elements: 31476

Total number of nodes: 92746



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Diab





Thermoelastic effect in FE model

Fortran user subroutine (developed in [2]) is used to generate synthetic TSA data

As an addition to the model, heat transfer is allowed at the debond region by using thermal contact.

• Teflon PTFE thermal properties



[2] Cappello, R., Pitarresi, G., Catalanotti, G.: Thermoelastic Stress Analysis for composite laminates: A numerical investigation. Compos Sci Technol. 241, 110103 (2023).https://doi.org/10.1016/J.COMPSCITECH.2023.110103









FE and Experiment (Full-field ΔT)



FE and Experiment (ΔT)













∆T -Through–thickness study (FE)





- 1 million Hz adiabatic response
- ΔT interface discontinuity is largest
- As heat transfer increases, these difference is reduced

When heat transfer occurs

Core is the heat source









Summary and Future work

General agreement between FE and experimental results

• Adopting DIC for motion compensation

FE results

- As the loading frequency increases
 - High thermoelastic responses move from the core to the interface
- Core material is the heat source

Potential of correlating the surface thermoelastic response with damage severity







