





Bayesian Calibration of a Geometrically Nonlinear Finite Element C-spar Model using Digital Image Correlation

Carl Scarth¹, Geir Olafsson², Janice M. Dulieu-Barton², Andrew T. Rhead¹, Richard Butler¹

¹Centre for Integrated Materials, Processes and Structures, University of Bath, Bath, UK
² Bristol Composites Institute, University of Bristol, Bristol, UK

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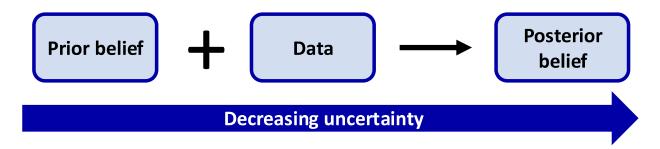




Background



- All predictions made by engineers are subject to uncertainty:
 - Manufacturing uncertainty
 - How accurate are models?
 - How representative are physical tests of reality?
 - Unknown quantities e.g. internal defects/features, damage
- Bayesian inference helps us quantify, and reduce this uncertainty using new data



• **Calibration** is a way of using experimental data to inform future model predictions while accounting for unknown model inputs





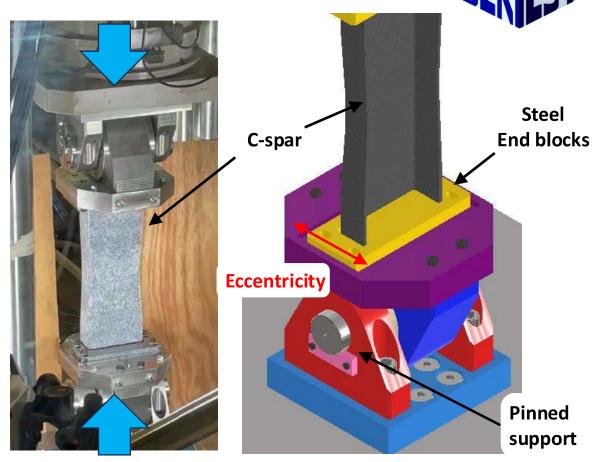


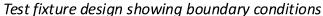




Problem Specification

- Stereo DIC from Compression tests on a C-spar undertaken at University of Bristol using MatchID.
- Focus on longitudinal displacement on external corner.
- +4mm load eccentricity relative to gauge section centroid.
- ABAQUS model with material, boundary condition, and geometric uncertainty.
- Can we use the test data to assess model accuracy given this uncertainty?
- Main challenge is using large volumes of DIC data spanning both time and space, to calibrate full-field model output.











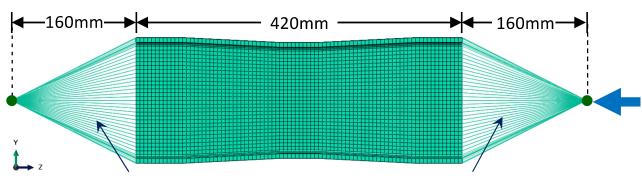




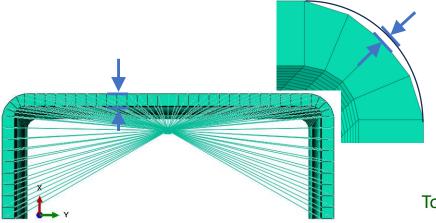
ABAQUS Model and Uncertainties



- Modelled with 4536 SC8R continuum shell elements (9354 nodes).
- Simply supported at reference nodes offset from spar.
- Uncertainty in boundary conditions.
- Geometric uncertainty in (ply) thickness and corner thinning.
- Uncertainty in longitudinal modulus E₁₁.



Truss elements with uncertain stiffness (K_{truss}) model rig compliance





Torsional springs with uncertain stiffness (K_{spring}) model resistance at bearing









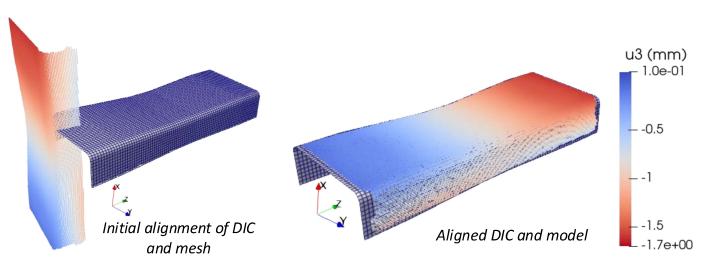


Alignment of DIC and model

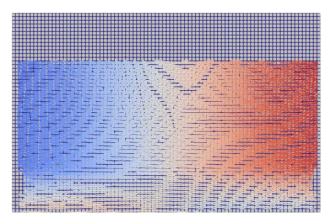


Set of tools developed (or adopted) for mapping DIC onto an ABAQUS mesh and making pointwise comparisons:

- 1) Point-cloud/mesh registration in CloudCompare¹.
- 2) Newton-Raphson method to transform from Cartesian coordinates to local element coordinates.
- 3) Interpolation across spatial domain using ABAQUS shape functions.
- 4) Linear interpolation across time domain to match solver increments.



Cartesian coordinates (x_i, y_i, z_i) (x_i, y_i, z_i)



DIC data transformed into element coordinates, arranged in regular grid.













Calibration: Methodology



• Following Higdon et al.², method for calibrating models with vector-valued output:

$$y = \eta(\theta^*) + \varepsilon$$
DIC point cloud Abaqus model Erro

 θ^* = uncertain inputs we want to learn about:

E₁₁, ply thickness, eccentricity bias, K_{truss}, radius thinning, K_{spring}

- An inverse problem:
 - -y is known.
 - $\boldsymbol{\theta}^*$ and magnitude of error $\boldsymbol{\varepsilon}$ are uncertain.
 - Gaussian process emulator used as surrogate for Abaqus, η , which also has uncertain parameters.
- Infer values for uncertain parameters by first specifying prior distributions.
- Then sample from the posterior distribution using Hamiltonian Monte Carlo (No-U-Turn Sampler, NUTS) in Stan³.

³ Stan modeling language users guide and reference manual, Version 2.26.1, https://mc-stan.org









² D. Higdon et al, "Computer model calibration using high-dimensional output", Journal of the American Statistical Association, 2008



Calibration: Prior distributions



Prior parameters: mean and standard deviation for Gaussian and Half-normal, upper and lower bounds for uniform

	E ₁₁ (GPa)	t _{ply} (mm)	Eccentricity bias (mm)	log(K _{truss})	Radius thinning (mm)	log(K _{spring})
Distribution	Gaussian	Gaussian	Gaussian	Uniform	Half-normal	Half-normal
Parameter 1	140.9	0.125	0.0	5.5	0.0	0.0
Parameter 2	8.454	0.005	0.667	18.0	0.667	2.0

- What do I **believe** about the uncertain inputs before the test?
- Not a measure of variability
- Rig stiffness, K_{truss} based on parametric study of initial gradient of force-displacement curves.
- Compressive modulus E₁₁ taken from published coupon test data⁴. Hexcel state 150GPa⁵. Which value is correct?

Initial gradient of force-displacement curve at reference node, vs log of rig stiffness

⁵ HexTow[®] IM7 Carbon Fibre, Product Data Sheet, HEXCEL









Wy 30 0.04 prior P

⁴E. Clarkson. "Hexcel 8552 IM7 unidirectional prepreg 190 gsm & 35% qualification statistical analysis report." NCAMP, 2019.

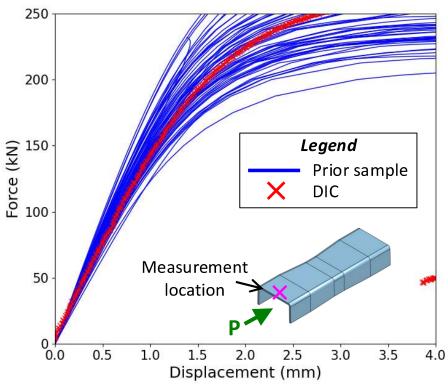




- Surrogate model fitted to ABAQUS output from 60 Latin Hypercube samples across input prior distributions.
- Decompose output into p = 16 principal components via SVD²:

$$\eta(\boldsymbol{\theta}^*) \approx \sum_{i=1}^p \boldsymbol{\phi}_i(\boldsymbol{x}, t) w_i(\boldsymbol{\theta}^*)$$

• Basis vectors ϕ_i capture spatial and temporal dependency.



Force vs displacement at point on web for training samples and DIC









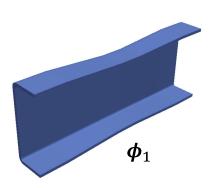


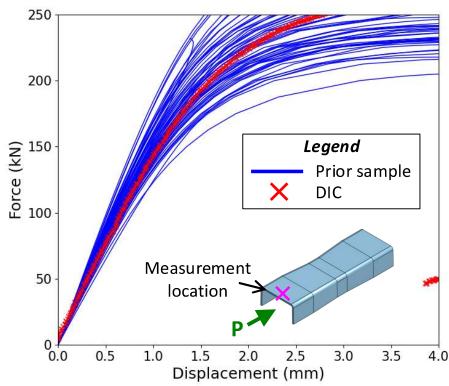


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Force vs displacement at point on web for training samples and DIC

First three basis vectors for emulator









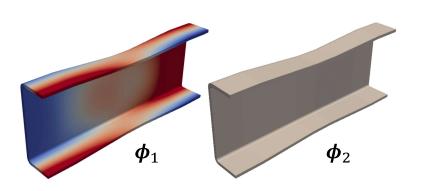




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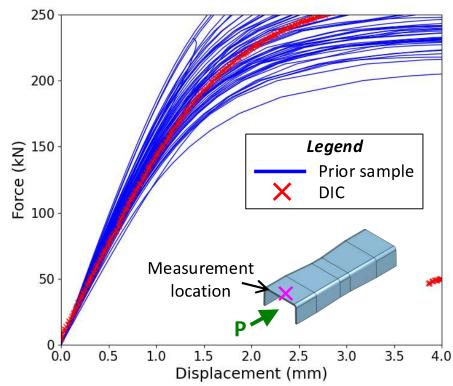


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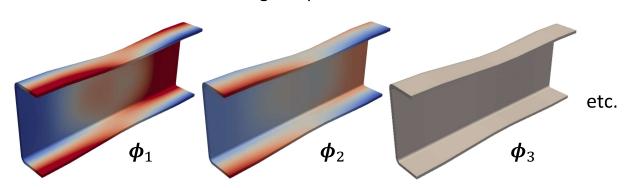




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- Basis vectors ϕ_i capture spatial and temporal dependency.
- Gaussian process emulators w_i model uncertain input dependency.
- Need to truncate output to 200kN so solver converges at all increments for all training samples.



250 200 Force (KN) 100 Legend Prior sample DIC Measurement 50 location 0.0 0.5 1.0 1.5 2.5 3.5 2.0 3.0 4.0 Displacement (mm)

Force vs displacement at point on web for training samples and DIC

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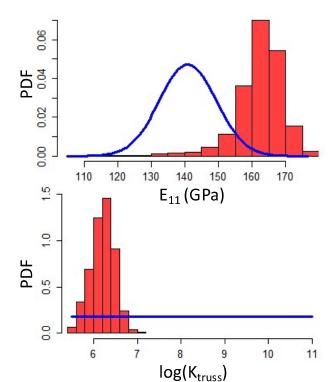


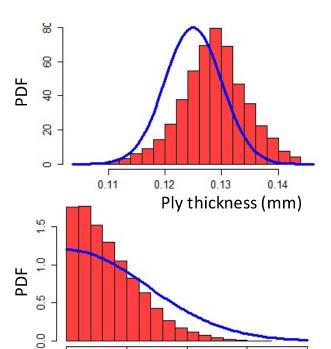






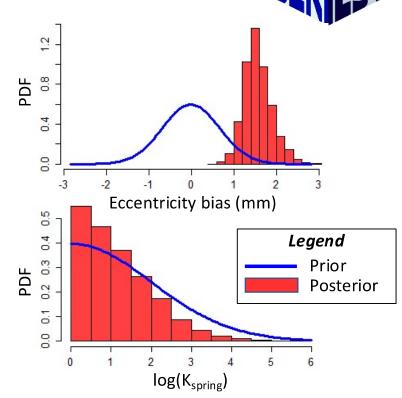
Results: Posterior distributions





1.0

Radius thinning (mm)







0.5

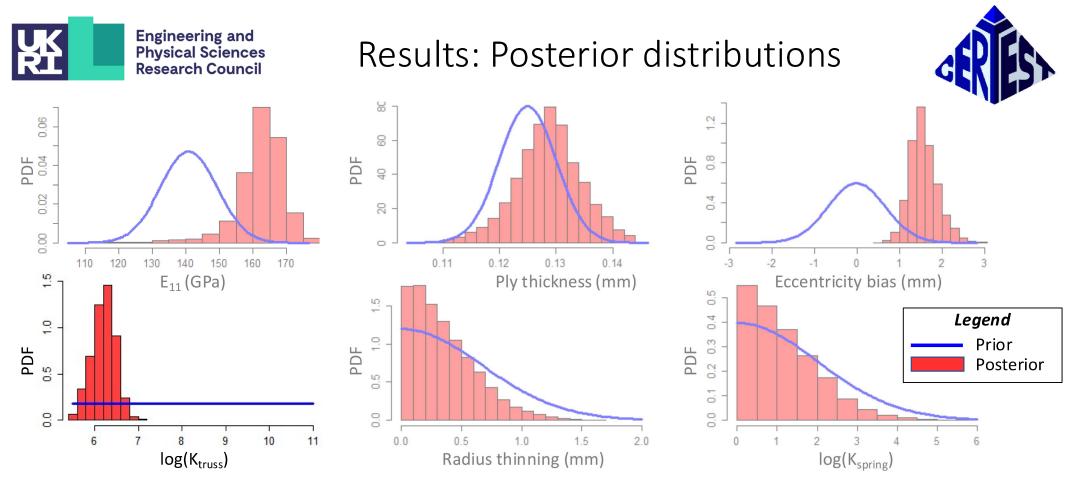
0.0



1.5

2.0





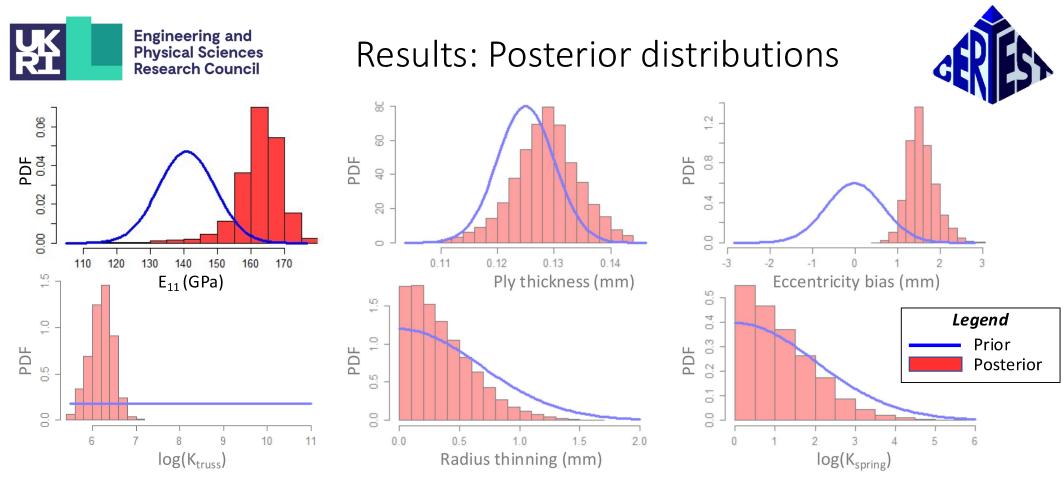
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- \bullet E₁₁ shifts towards higher values, with mode of 164 GPa similar to tensile modulus.



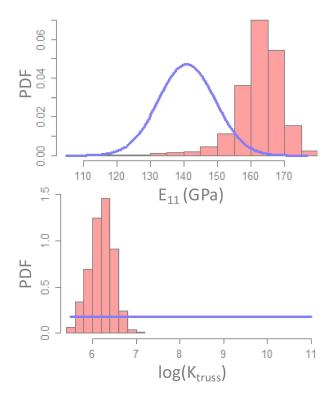


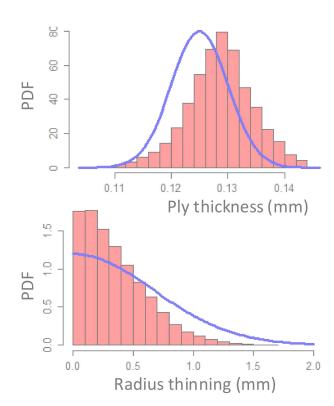


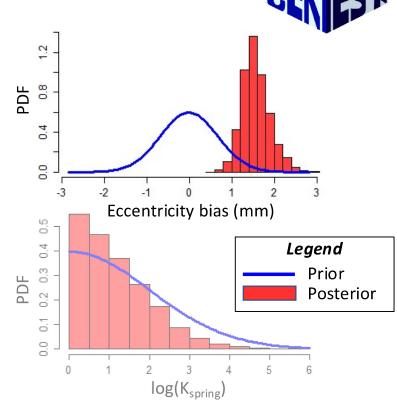




Results: Posterior distributions







- K_{truss} shifts to very low values (approx. 40% knockdown in overall stiffness) indicating significant rig or machine compliance.
- \bullet E₁₁ shifts towards higher values, with mode of 164 GPa similar to tensile modulus.
- Strong shift of loading axis via eccentricity bias, which later highlighted a manufacturing error.







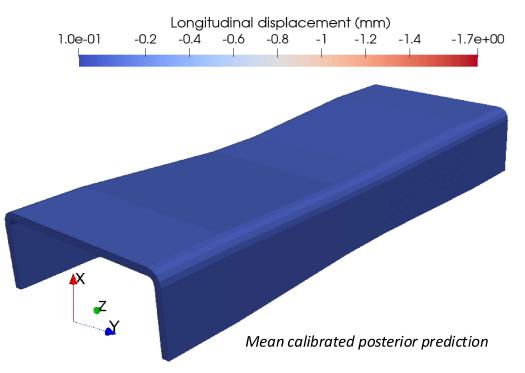




Results: Calibrated predictions



• Run posterior samples through emulator and average out uncertainty to get prediction.









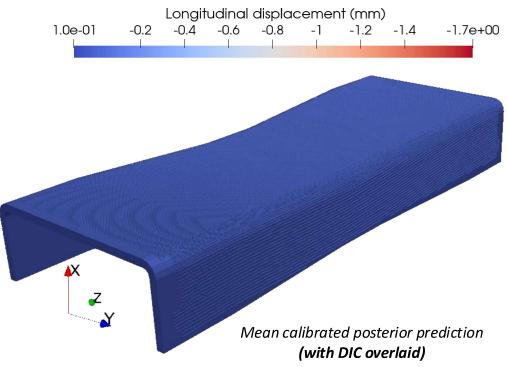




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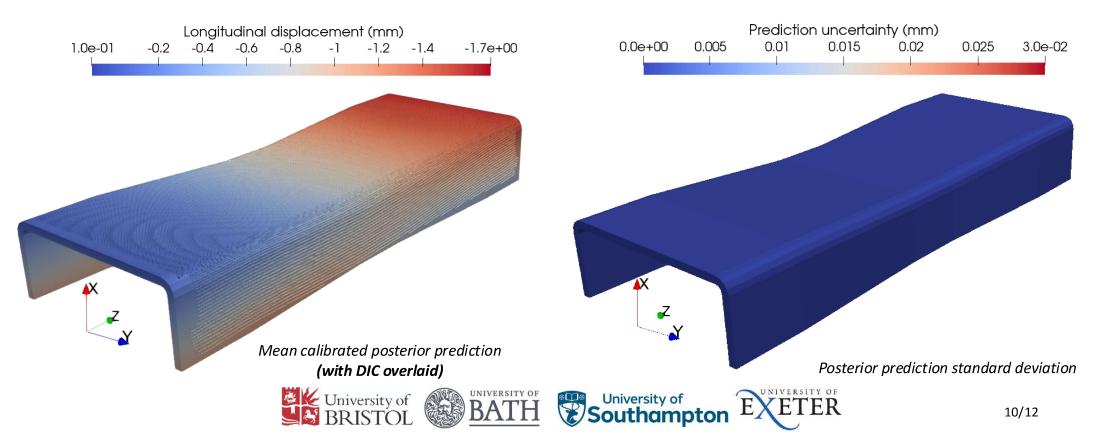




Results: Calibrated predictions



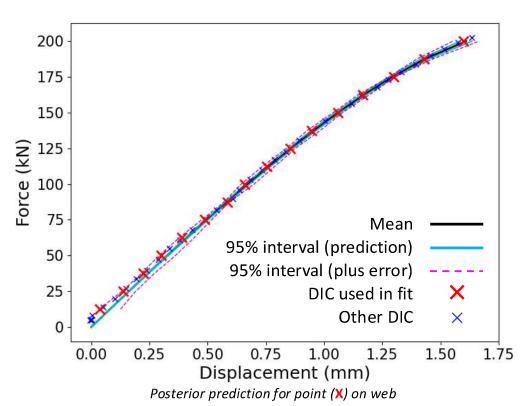
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- Standard deviation indicates regions of highest posterior uncertainty.

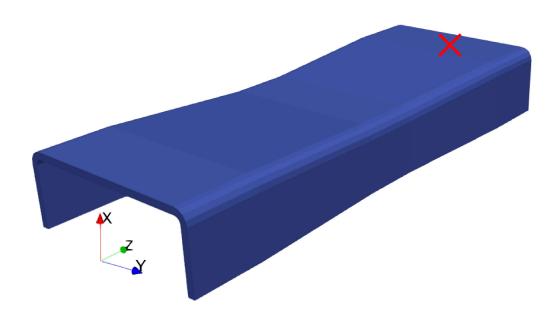






• Extract force-displacement at fixed location to visualise fit









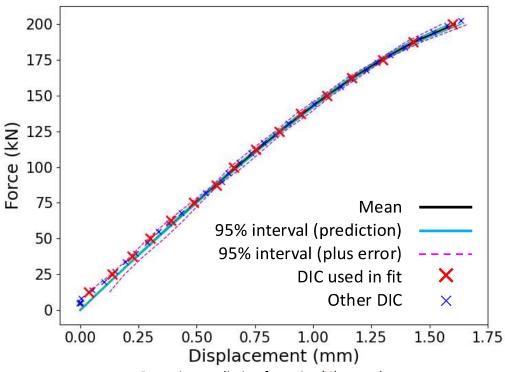








- Extract force-displacement at fixed location to visualise fit
- Subtract the DIC from each increment of calibrated model to visualise residuals highlighting regions of discrepancy.

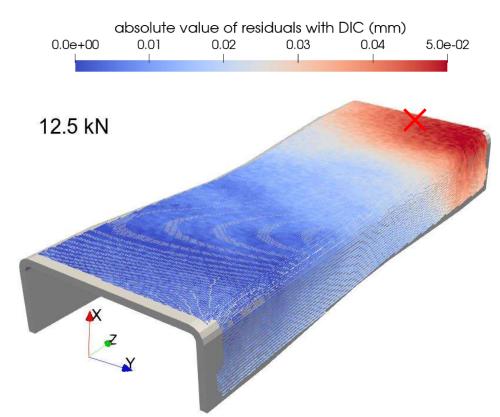


Posterior prediction for point (X) on web







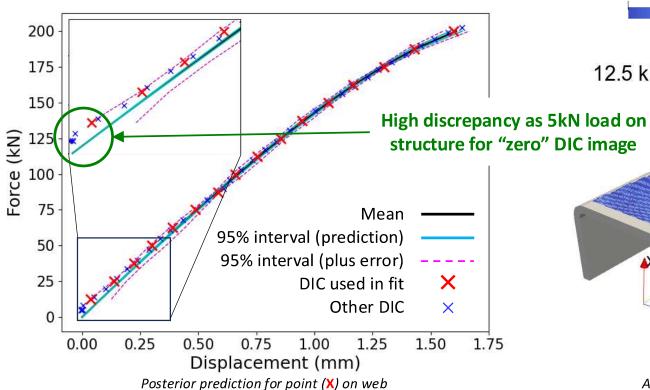


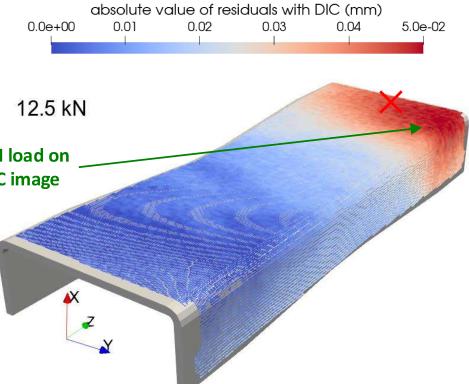
Absolute residual of mean prediction compared with DIC





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Absolute residual of mean prediction compared with DIC





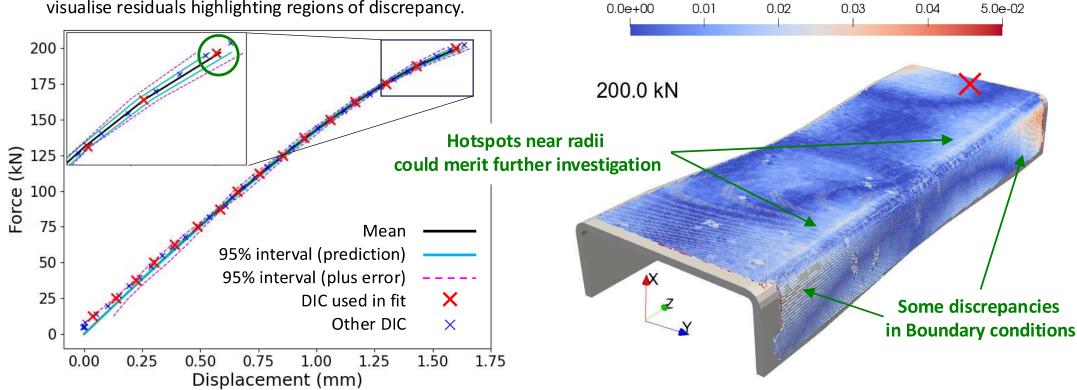




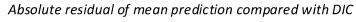




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Posterior prediction for point (X) on web



absolute value of residuals with DIC (mm)











Conclusions and future work



- Demonstrated a powerful statistical toolkit for comparing FE models against DIC while accounting for uncertainty in model inputs and test data.
- Overcame challenge of calibrating full-field output using high volumes of data.
- Uncertainty in boundary conditions very important.
- Highlighted manufacturing error helping with ongoing model validation.
- Future work could include:
 - Using full displacement vector.





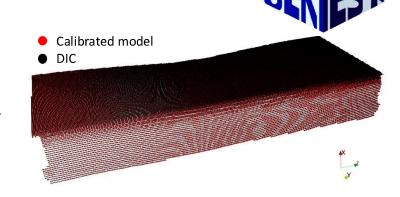




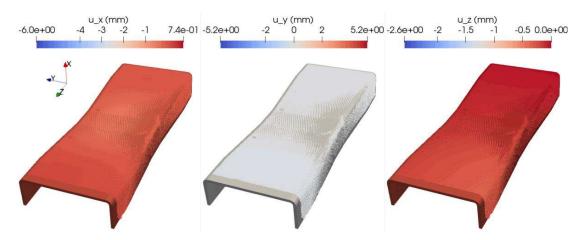


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- Uncertainty in boundary conditions very important.
- Highlighted manufacturing error helping with ongoing model validation.
- Future work could include:
 - Using full displacement vector.
 - More complex phenomena such as failure.
 - Use in model validation
 - Informing future choice of experiments.



DIC vs model point cloud with discrepancy in boundary



DIC overlaid on calibrated model predictions for historic test data









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Alan Turing

Institute

























Thank you for listening!

Any questions?







