



Engineering and  
Physical Sciences  
Research Council



# Enhanced Performance and Productivity via Integration of Multi-scale Modelling

1<sup>st</sup> August 2023

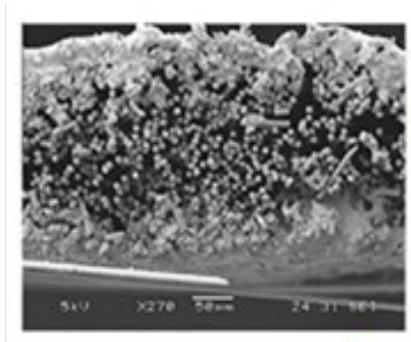
*Richard Butler, University of Bath, UK*

University of  
BRISTOL

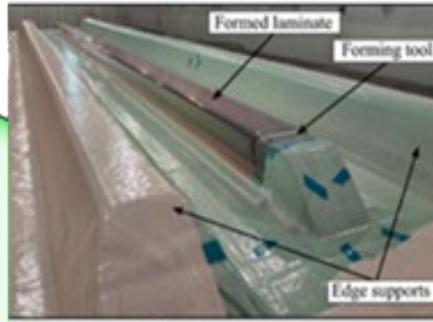


# Motivation

How do we fully exploit performance and productivity of composites?



Material  
Characterisation



Productivity-driven composite parts requires full integration of materials, manufacturing and structures

Structural  
Performance

Manufacturing  
Process



# Overview

- Part **Formability** – opportunities of non-standard ply angles
- Coupon-level testing – limitations of “Black Metal” approach to certification
- Multiscale modelling: a new pathway to part-level design and certification?

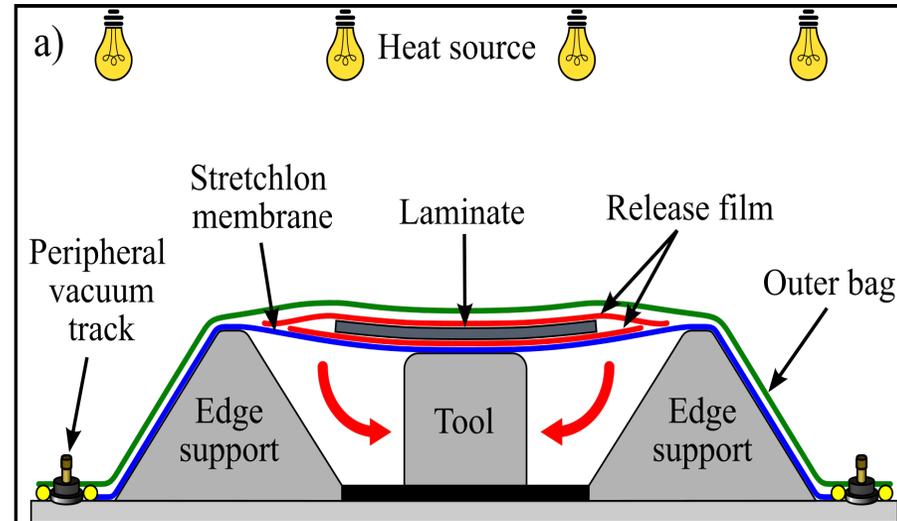
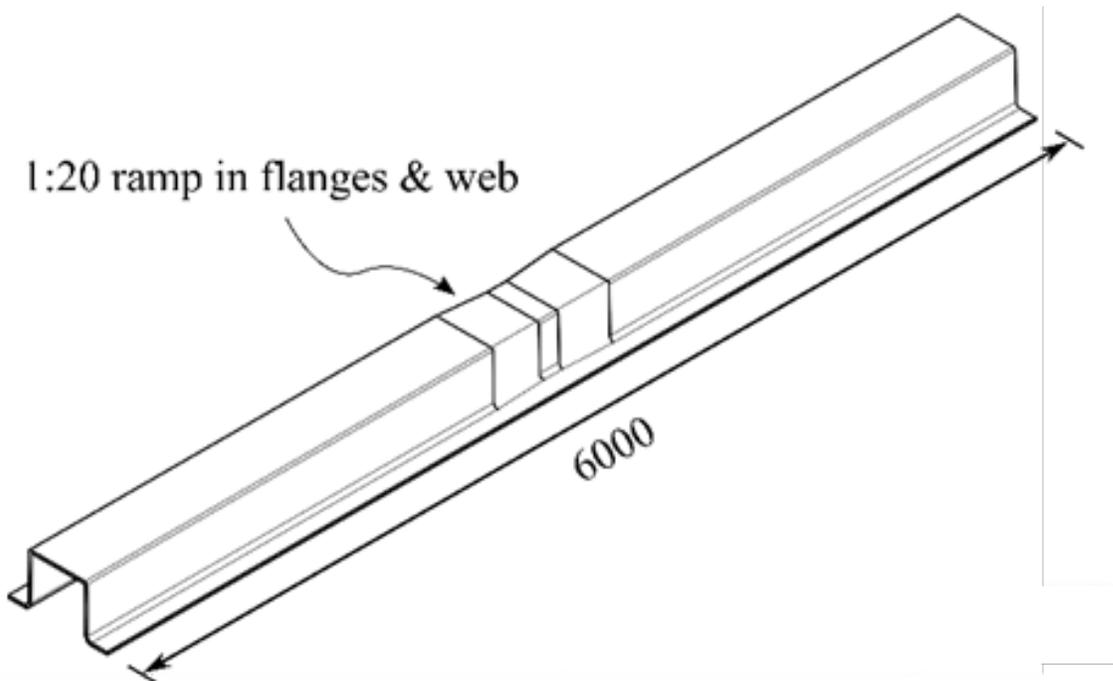
# Formability

- Forming from flat can increase production rate
- Difficult for complex geometry in long parts
- New laminate design methodologies to improve formability via compatibility index  $C_{max}$  [1]
- Investigated length effect in forming of parts with long fibres [2]

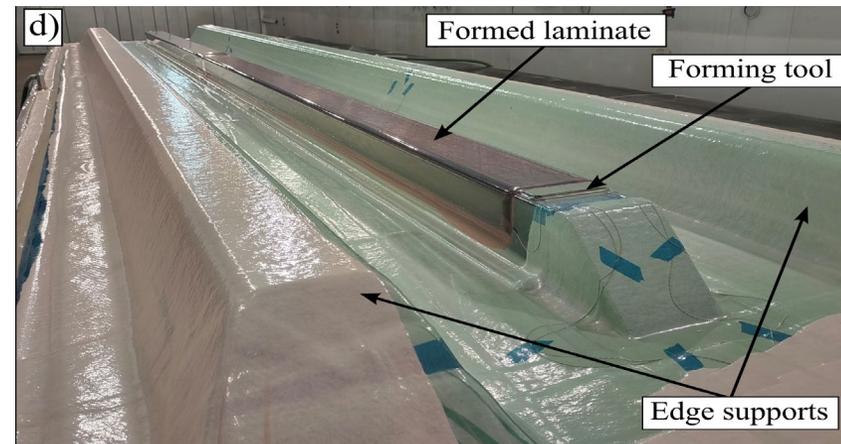
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1. Johnson et al, Composites Science & Technology, 2019
  2. Scarth et al, Composites: Part B, 2023

# Formability- length effect

- 6m long C-spars with mid-length recess formed at National Composites Centre
- UD pre-preg material
- Three stacking sequences; standard and non-standard ply angles

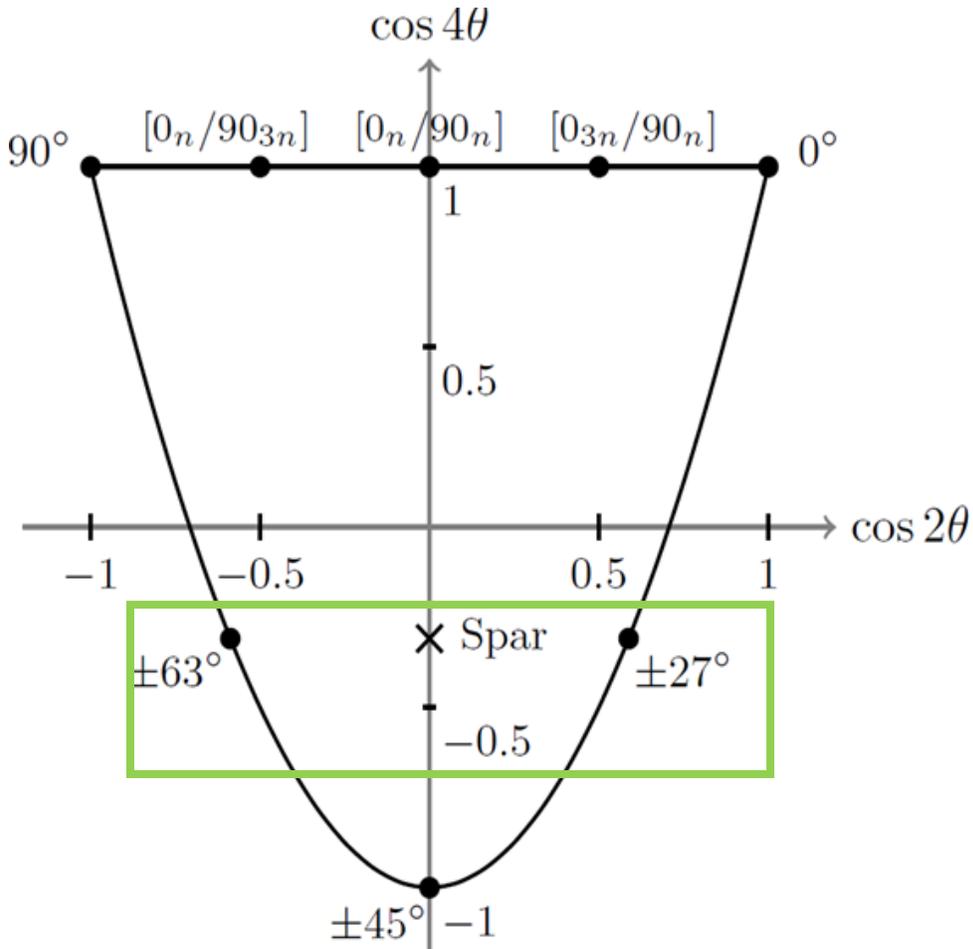


Forming setup



Formed part

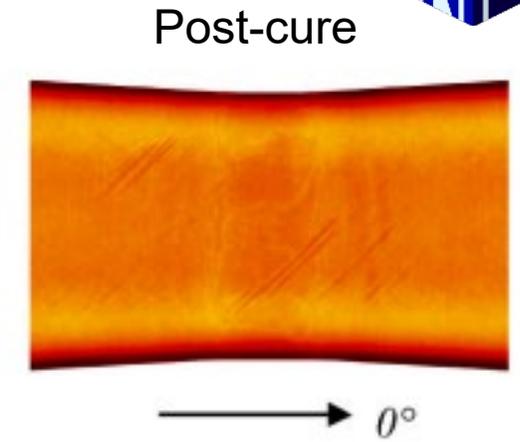
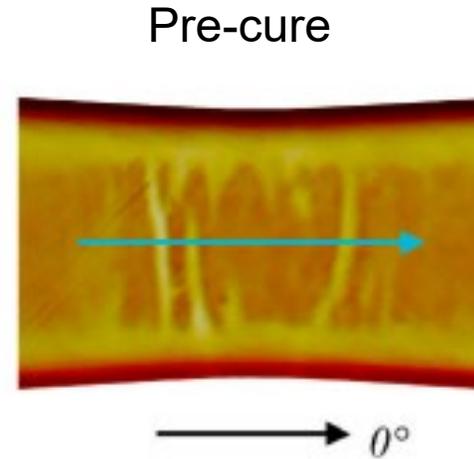
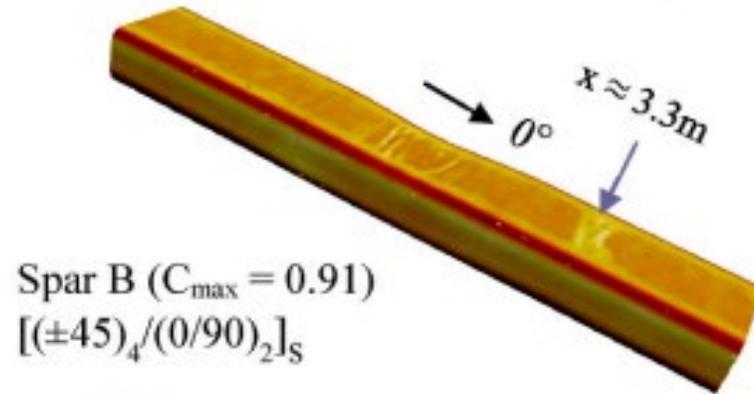
# Formability – laminate design



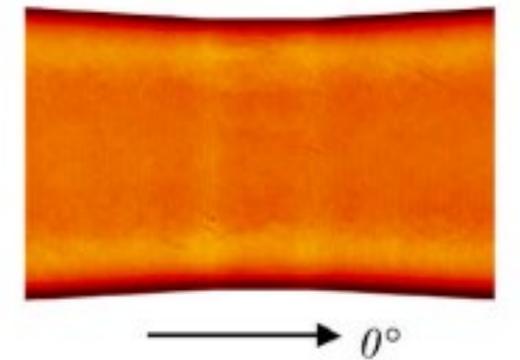
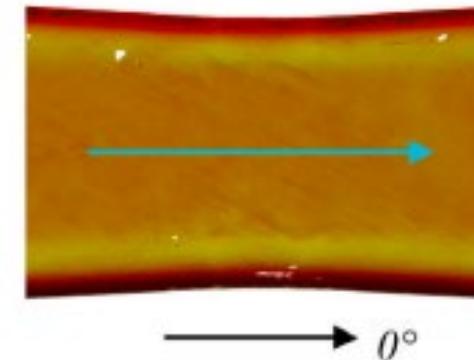
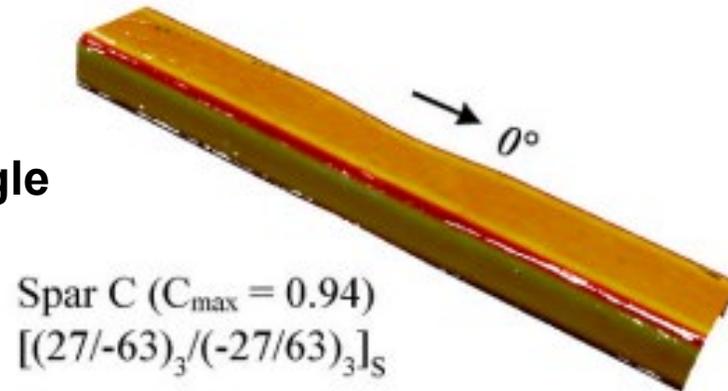
- In-plane stiffness is defined by linear combinations of two lamination parameters  $\cos 4\theta$  and  $\cos 2\theta$
- 50/50 (%  $\pm 27^\circ/\pm 63^\circ$ ) has same in-plane stiffness as a standard angle spar laminate – e.g. 17/66/17 (%  $0^\circ/\pm 45^\circ/90^\circ$ )
- Non-Standard angle laminate has reduce fibre length effect – improve formability

# Post forming - surface scans

## Standard Angle Laminate



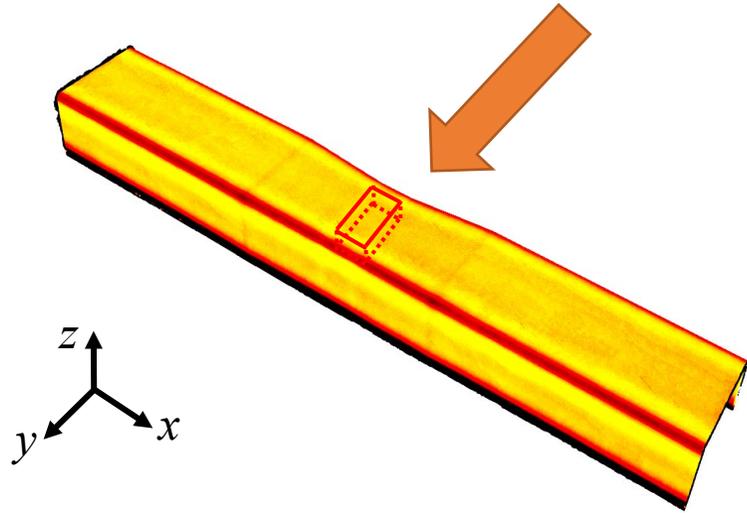
## Non-standard Angle Laminate



- Standard angle laminate (6m long  $0^\circ$  fibres) has transverse wrinkles
- Non-standard angles (0.6m long  $27^\circ$  fibres) does not

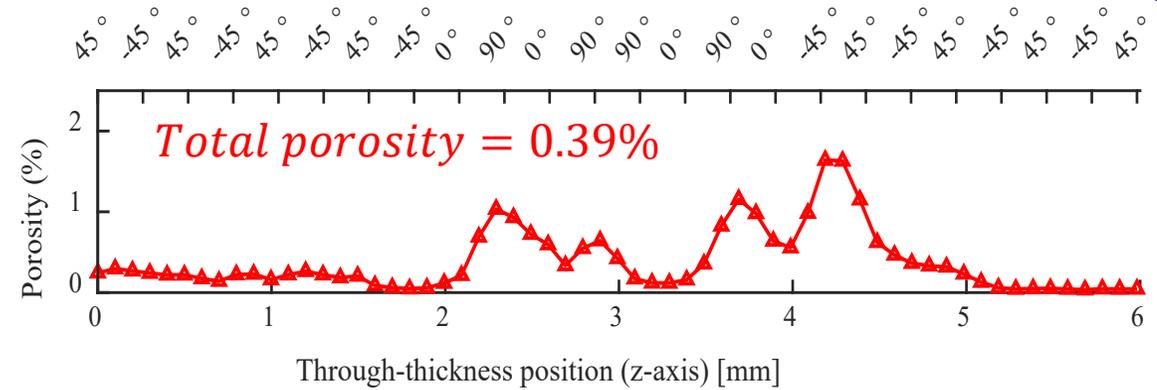
# Post-cure X-Ray CT

- Porosity in recess – centre of web

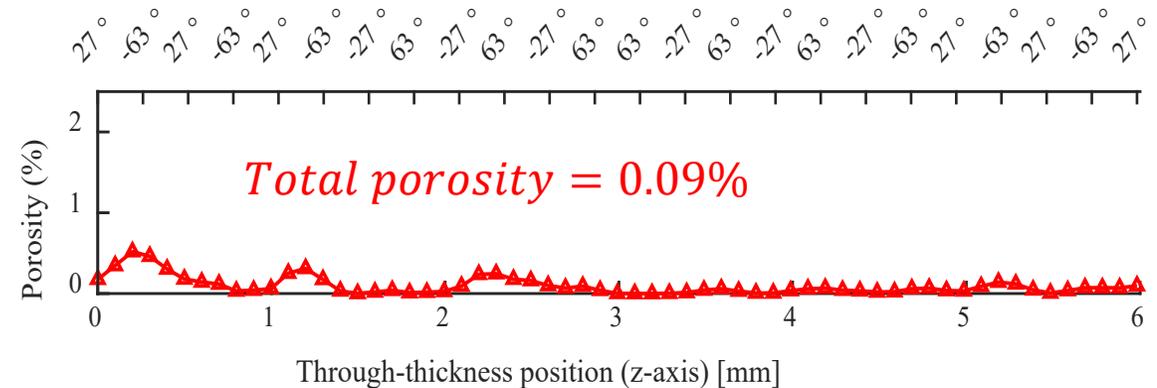


- Standard Angle laminate has 1-2% porosity in 0° plies
- Significantly lower porosity in Non-Standard Angle Laminate

## Standard Angle Laminate



## Non-Standard Angle Laminate



# Overview

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- **Coupon-level testing** – limitations of “Black Metal” approach to certification
- Multiscale modelling - a new pathway to part-level design and certification?

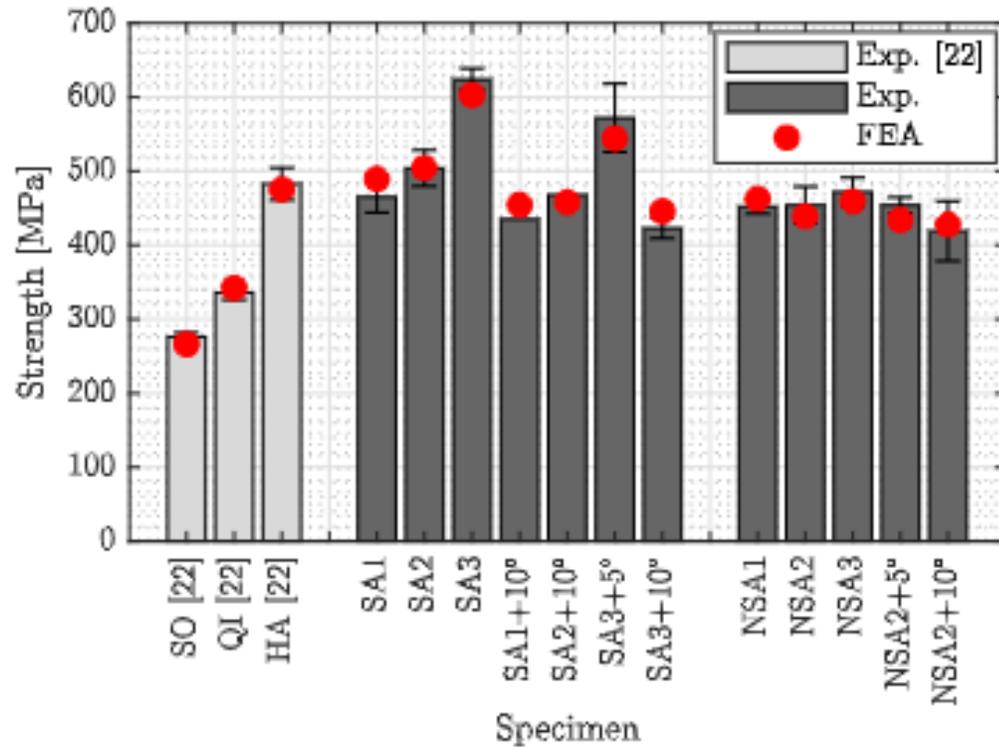
# Coupon testing: Open Hole Tension



Standard Angle laminate: 50/40/10 (0/±45/90)

Non-Standard Angle laminate: 60/40 (±10/±57)

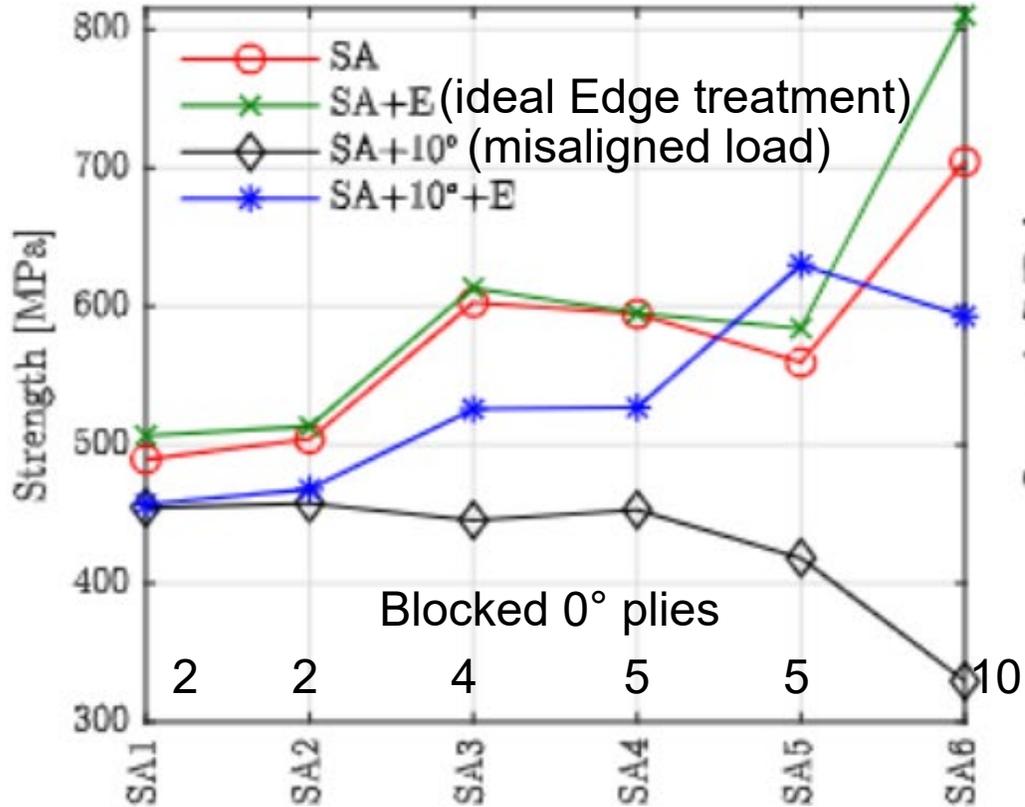
Equivalent in-plane stiffness (skin laminate)



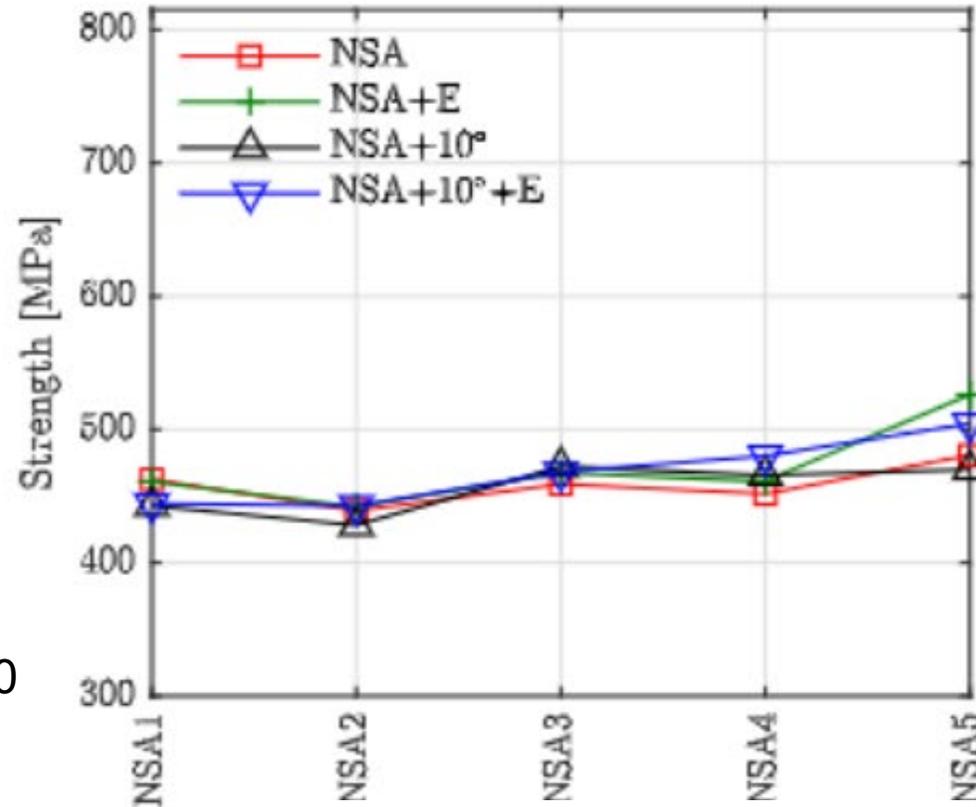
- [22] = Falco et al., Compos Struct, 2018.
- SA1; SA2 two blocked 0° plies
- SA3; four blocked 0° plies
- +10° = tension applied with 10° misalignment

\*Chuaqui et al, Composites B, 2021

# Virtual coupon testing



**Standard Angle laminates**



**Non-Standard Angle laminates**

Chuaqui et al,  
Composites B, 2021

- Shear load (misaligned tension) reduces strength by up to 60%
- Up to 50% recovery with numerical (ideal) edge treatment – edge failure prevented
- Non-standard angles less optimal but insensitive to misalignment and edge treatment

# Overview

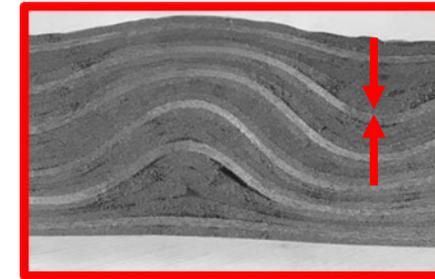
- Part Formability – opportunities of non-standard ply angles
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- **Multiscale modelling** - a new pathway to part-level design and certification?

# Multiscale modelling



## Motivation

- Coupon tests represent failure without any local/global interaction (“Black Metal” approach)
- Defects and failure of composite laminates can modelled at scale of layers and interlayers (**meso-scale, of order 10  $\mu\text{m}$** )
- How do we link this scale with structural performance of parts (**macro-scale, of order 1m**)?
- We are creating two approaches to Multiscale Modelling



# Multi-scale modelling

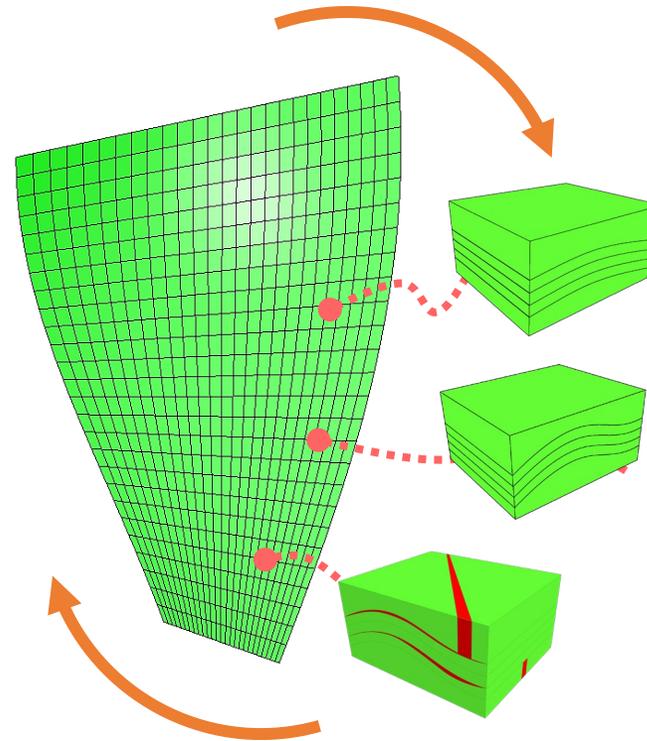
## 1. Framework for shell elements



**Scale transition:**  
Second-order homogenisation

**Downscaling:**  
Apply shell strains to the RVEs

**Upscaling:**  
Homogenise shell resultants and  
ABD + shear matrices

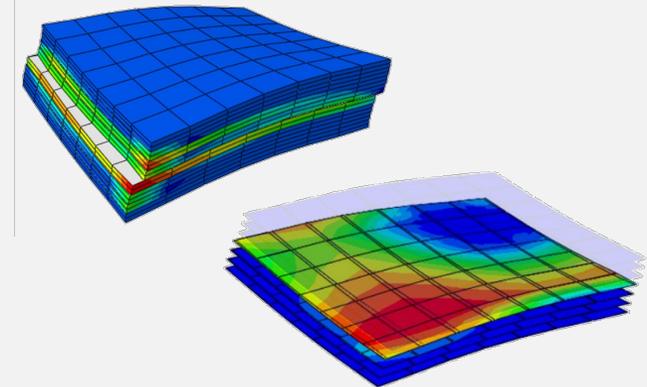


Macromodel: Shell elements

Mesomodel: Hi-fi solid RVE model

- Manufacturing defects
- Complex geometric features
- Progressive damage events

**Example RVE modes**

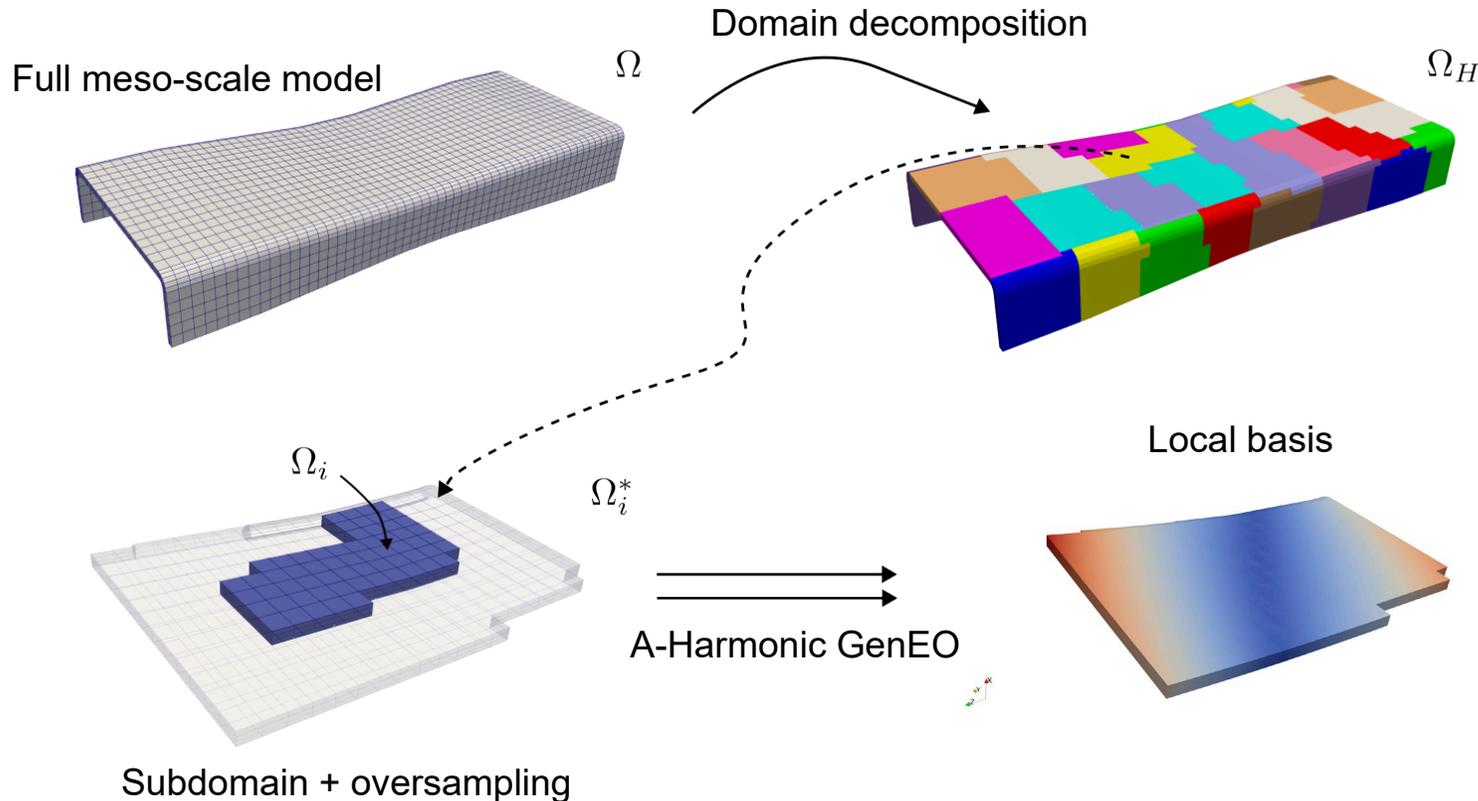


Inter + intralaminar damage progression

A.K.W. Hii, B. El Said, *A kinematically consistent second-order computational homogenisation framework for thick shell models*, Computer Methods in Applied Mechanics and Engineering, Volume 398, 2022

# Multiscale modelling

## 2. Spectral Generalized FEM



- **Partition of Unity** operator stitch subdomains
- **Oversampling** ease accuracy of coarse solution at interfaces
- Very **efficient and parallelized method** for nonlinear large scale problem
- **No scale separation:** various imperfection type / size / shape

Bénézech, J, et al. Scalable multiscale-spectral GFEM with an application to composite aero-structures, 2023, submitted to JCP <https://doi.org/10.48550/arXiv.2211.13893>

# Conclusions



- The **great challenge**: produce radically new high-performance products with reduced time to market
- Fundamental significance of **manufacturing process** on **material characterisation** and **structural performance**
- Alignment and length of **fibres**, and **matrix** constitution within the final product is critical
- The **current Building Block** approach, underpinned by coupon testing, does not fully exploit design opportunities nor is it representative of in-situ strength
- New statistical methods must be created to design, model and test at the component level, safely accounting for **uncertainty** and exploiting new design opportunities including manufacturability.